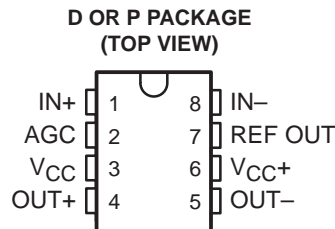


TL026C DIFFERENTIAL HIGH-FREQUENCY AMPLIFIER WITH AGC

SLFS007A – JUNE 1985 – REVISED JULY 1990

- Low Output Common-Mode Sensitivity to AGC Voltages
- Input and Output Impedances Independent of AGC Voltage
- Peak Gain . . . 38 dB Typ
- Wide AGC Range . . . 50 dB Typ
- 3-dB Bandwidth . . . 50 MHz
- Other Characteristics Similar to NE592 and uA733



description

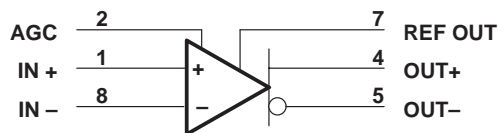
This device is a monolithic two-stage high-frequency amplifier with differential inputs and outputs.

Internal feedback provides wide bandwidth, low phase distortion, and excellent gain stability. Variable gain based on signal summation provides large AGC control over a wide bandwidth with low harmonic distortion. Emitter-follower outputs enable the device to drive capacitive loads. All stages are current-source biased to obtain high common-mode and supply-voltage rejection ratios. The gain may be electronically attenuated by applying a control voltage to the AGC pin. No external compensation components are required.

This device is particularly useful in TV and radio IF and RF AGC circuits, as well as magnetic-tape and disk-file systems where AGC is needed. Other applications include video and pulse amplifiers where a large AGC range, wide bandwidth, low phase shift, and excellent gain stability are required.

The TL026C is characterized for operation from 0°C to 70°C.

symbol



absolute maximum ratings over operating free-air temperature range (unless otherwise noted)†

| | |
|--|------------------------------|
| Supply voltage, V_{CC+} (see Note 1) | 8 V |
| Supply voltage, V_{CC-} (see Note 1) | - 8 V |
| Differential input voltage | ± 5 V |
| Common-mode input voltage | ± 6 V |
| Output current | ± 10 mA |
| Continuous total dissipation | See Dissipation Rating Table |
| Operating free-air temperature range | 0°C to 70°C |
| Storage temperature range | - 65°C to 150°C |
| Lead temperature range 1,6 mm (1/16 inch) from case for 10 seconds | 260°C |

† Stresses beyond those listed under absolute maximum ratings may cause permanent damage to the device. This is a stress rating only, and functional operation of the device at these or any other conditions beyond those indicated in the recommended operating conditions section of this specification is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

NOTE 1: All voltages are with respect to the midpoint of V_{CC+} and V_{CC-} except differential input and output voltages.

DISSIPATION RATING TABLE

| PACKAGE | $T_A \leq 25^\circ\text{C}$ POWER RATING | OPERATING FACTOR ABOVE $T_A = 25^\circ\text{C}$ | $T_A = 70^\circ\text{C}$ POWER RATING |
|---------|---|--|--|
| D | 725 mW | 5.8 mW/°C | 464 mW |
| P | 1000 mW | 8.0 mW/°C | 640 mW |

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recommended operating conditions

| | MIN | NOM | MAX | UNIT |
|---|-----|-----|-----|------|
| Supply voltage, V_{CC+} | 3 | 6 | 8 | V |
| Supply voltage, V_{CC-} | -3 | -6 | -8 | V |
| Operating free-air temperature range, T_A | 0 | | 70 | °C |

electrical characteristics at 25°C operating free-air temperature, $V_{CC+} = \pm 6V$, $V_{AGC} = 0$, REF OUT pin open (unless otherwise specified)

| PARAMETER | FIGURE | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
|-----------------|--------|--|---------|------|------|-----------|
| A_{VD} | 1 | $V_{O(PP)} = 3V$, $R_L = 2k\Omega$ | 65 | 85 | 105 | V/V |
| ΔA_{VD} | 1 | $V_{I(PP)} = 28.5mV$, $R_L = 2k\Omega$, $V_{AGC} - V_{ref} = \pm 180mV$ | | -50 | | dB |
| V_{ref} | | $I_{ref} = -1mA$ to $100\mu A$ | 1.3 | | 1.5 | V |
| BW | 2 | $V_{O(PP)} = 1V$, $V_{AGC} - V_{ref} = \pm 180mV$ | | 50 | | MHz |
| I_{IO} | | | | 0.4 | 5 | μA |
| I_{IB} | | | | 10 | 30 | μA |
| V_{ICR} | 3 | | ± 1 | | | V |
| V_{OC} | 1 | $R_L = \infty$ | 3.25 | 3.75 | 4.25 | V |
| ΔV_{OC} | 1 | $V_{AGC} = 0$ to $2V$, $R_L = \infty$ | | | 300 | mV |
| V_{OO} | 1 | $V_{ID} = 0$, $R_L = \infty$ | | | 0.75 | V |
| $V_{O(PP)}$ | 1 | $R_L = 2k\Omega$ | 3 | 4 | | V |
| r_i | | | 10 | 30 | | $k\Omega$ |
| r_o | | | | 20 | | Ω |
| CMRR | 3 | $V_{IC} = \pm 1V$, $f = 100kHz$ | 60 | 86 | | dB |
| | | $V_{IC} = \pm 1V$, $f = 5mHz$ | | 60 | | |
| k_{SVR} | 4 | $\Delta V_{CC+} = \pm 0.5V$, $\Delta V_{CC-} = \pm 0.5V$ | 50 | 70 | | dB |
| V_n | 4 | BW = 1 kHz to 10 MHz | | 12 | | μV |
| t_{pd} | 2 | $\Delta V_O = 1V$ | | 6 | 10 | ns |
| t_r | 2 | $\Delta V_O = 1V$ | | 4.5 | 12 | ns |
| $I_{sink(max)}$ | | $V_{ID} = 1V$, $V_O = 3V$ | 3 | 4 | | mA |
| I_{CC} | | No load, No signal | | 22 | 27 | mA |



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electrical characteristics over recommended operating free-air temperature range, $V_{CC\pm} = \pm 6\text{ V}$, $V_{AGC} = 0$, REF OUT pin open (unless otherwise specified)

| PARAMETER | FIGURE | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
|--|--------|--|---------|-----|-----|------------------|
| A_{VD} Large-signal differential voltage amplification | 1 | $V_{O(PP)} = 3\text{ V}$, $R_L = 2\text{ k}\Omega$ | 55 | | 115 | V/V |
| I_{IO} Input offset current | | | | | 6 | μA |
| I_{IB} Input bias current | | | | | 40 | μA |
| V_{ICR} Common-mode input voltage range | 3 | | ± 1 | | | V |
| V_{OO} Output offset voltage | 1 | $V_{ID} = 0$, $R_L = \infty$ | | | 1.5 | V |
| $V_{O(PP)}$ Maximum peak-to-peak output voltage swing | 1 | $R_L = 2\text{ k}\Omega$ | 2.8 | | | V |
| r_i Input resistance at AGC, IN+, or IN- | | | 8 | | | $\text{k}\Omega$ |
| CMRR Common-mode rejection ratio | 3 | $V_{IC} = \pm 1\text{ V}$, $f = 100\text{ kHz}$ | 50 | | | dB |
| k_{SVR} Supply voltage rejection ratio ($\Delta V_{CC} / \Delta V_{IO}$) | 4 | $\Delta V_{CC+} = \pm 0.5\text{ V}$, $\Delta V_{CC-} = \pm 0.5\text{ V}$ | 50 | | | dB |
| $I_{\text{sink(max)}}$ Maximum output sink current | | $V_{ID} = 1\text{ V}$, $V_O = 3\text{ V}$ | 2.8 | 4 | | mA |
| I_{CC} Supply current | 1 | No load, No signal | | | 30 | mA |

PARAMETER MEASUREMENT INFORMATION

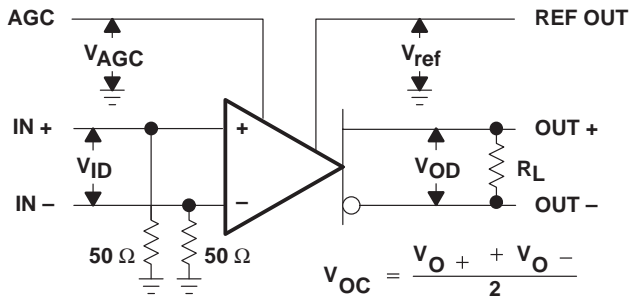


Figure 1. Test Circuit

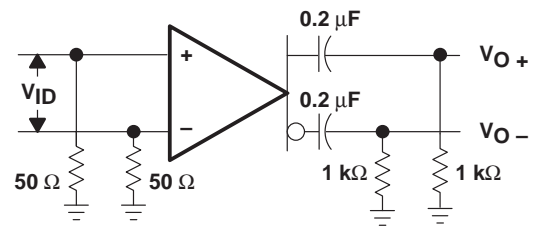


Figure 2. Test Circuit

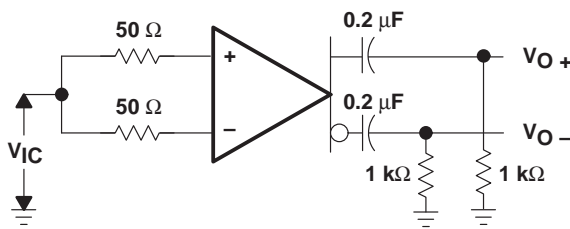


Figure 3. Test Circuit

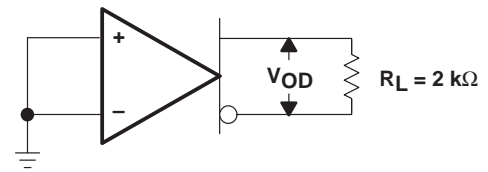


Figure 4. Test Circuit

TL026C DIFFERENTIAL HIGH-FREQUENCY AMPLIFIER WITH AGC

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TYPICAL CHARACTERISTICS

DIFFERENTIAL VOLTAGE AMPLIFICATION
vs
DIFFERENTIAL GAIN-CONTROL VOLTAGE

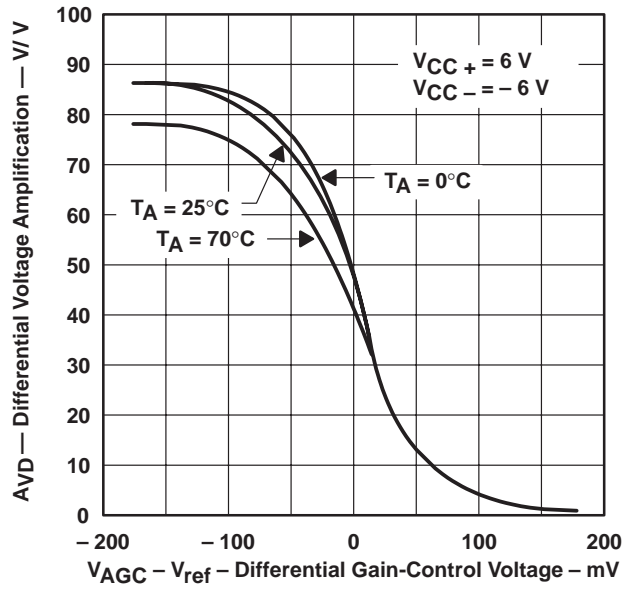


Figure 5

APPLICATION INFORMATION

gain characteristics

Figure 5 shows the differential voltage amplification versus the differential gain-control voltage ($V_{AGC} - V_{ref}$). V_{AGC} is the absolute voltage applied to the A_{GC} input and V_{ref} is the dc voltage at the REF OUT output. As V_{AGC} increases with respect to V_{ref} , the TL026C gain changes from maximum to minimum. As shown in Figure 5 for example, V_{AGC} would have to vary from approximately 180 mV less than V_{ref} to approximately 180 mV greater than V_{ref} to change the gain from maximum to minimum. The total signal change in V_{AGC} is defined by the following equation.

$$\begin{aligned}\Delta V_{AGC} &= V_{ref} + 180 \text{ mV} - (V_{ref} - 180 \text{ mV}) \\ \Delta V_{AGC} &= 360 \text{ mV}\end{aligned}\tag{1}$$

However, because V_{AGC} varies as the ac AGC signal varies and also differentially around V_{ref} , then V_{AGC} should have an ac signal component and a dc component. To preserve the dc and thermal tracking of the device, this dc voltage must be generated from V_{ref} . To apply proper bias to the AGC input, the external circuit used to generate V_{AGC} must combine these two voltages. Figures 6 and 7 show two circuits that will perform this operation and are easy to implement. The circuits use a standard dual operational amplifier for AGC feedback. By providing rectification and the required feedback gain, these circuits are also complete AGC systems.

circuit operation

Amplifier A1 amplifies and inverts the rectified and filtered AGC signal voltage V_C producing output voltage V_1 . Amplifier A2 is a differential amplifier that inverts V_1 again and adds the scaled V_{ref} voltage. This conditioning makes V_{AGC} the sum of the signal plus the scaled V_{ref} . As the signal voltage increases, V_{AGC} increases and the gain of the TL026C is reduced. This maintains a constant output level.

feedback circuit equations

Following the AGC input signal (Figures 6 and 7) from the OUT output through the feedback amplifiers to the AGC input produces the following equations:

1. AC output to diode D1, assuming sinusoidal signals

$$V_O = V_{OP} (\sin (wt))\tag{2}$$

where:

$$V_{OP} = \text{peak voltage of } V_O$$

2. Diode D1 and capacitor C1 output

$$V_C = V_{OP} - V_F\tag{3}$$

where:

$$V_F = \text{forward voltage drop of D1}$$

$$V_C = \text{voltage across capacitor C1}$$

3. A1 output

$$V_1 = - \frac{R_2}{R_1} V_C\tag{4}$$

4. A2 output ($R_3 = R_4$)

$$V_{AGC} = \frac{R_2}{R_1} V_C + 2 \frac{R_6}{R_5 + R_6} V_{ref}\tag{5}$$

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Amplifier A2 inverts V1 producing a positive AGC signal voltage. Therefore, the input voltage to the TL026C AGC pin consists of an AGC signal equal to:

$$\frac{R2}{R1} V_C \quad (6)$$

and a dc voltage derived from V_{ref} , defined as the quiescent value of V_{AGC} .

$$V_{AGC}(q) = 2 \frac{R6}{R5 + R6} V_{ref} \quad (7)$$

For the initial resistor calculations, V_{ref} is assumed to be typically 1.4 V making quiescent V_{AGC} approximately 1.22 V ($V_{AGC}(q) = V_{ref} - 180$ mV). This voltage allows the TL026C to operate at maximum gain under no-signal and low-signal conditions. In addition, with V_{ref} used as both internal and external reference, its variation from device to device automatically adjusts the overall bias and makes AGC operation essentially independent of the absolute value of V_{ref} . The resistor divider needs to be calculated only once and is valid for the full tolerance of V_{ref} .

output voltage limits (see Figures 6 and 7)

The output voltage level desired must fall within the following limits:

1. Because the data sheet minimum output swing is 3 V peak-to-peak using a 2-k Ω load resistor, the user-selected design limit for the peak output swing should not exceed 1.5 V.
2. The voltage drop of the rectifying diode determines the lower voltage limit. When a silicon diode is used, this voltage is approximately 0.7 V. The output voltage V_O must have sufficient amplitude to exceed the rectifying diode drop. A Schottky diode can be used to reduce the V_O level required.

gain calculations for a peak output voltage of 1 V

A peak output voltage of 1 V was chosen for gain calculations because it is approximately midway between the limits of conditions 1 and 2 in the preceding paragraph.

Using equation 3 ($V_C = V_{OP} - V_d$), V_C is calculated as follows:

$$V_C = 1 \text{ V} - 0.7 \text{ V}$$

$$V_C = 0.3 \text{ V}$$

Therefore, the gain of A1 must produce a voltage V1 that is equal to or greater than the total change in V_{AGC} for maximum TL026C gain change.

With a total change in V_{AGC} of 360 mV and using equation 4, the calculation is as follows:

$$-\frac{V1}{V_C} = \frac{\Delta V_{AGC}}{V_C} = \frac{R2}{R1} = \frac{0.36}{0.3} = 1.2$$

If R1 is 10 k Ω , R2 is 1.2 times R1 or 12 k Ω .

Since the output voltage for this circuit must be between 0.85 V and 1.3 V, the component values in Figures 6 and 7 provide a nominal 1-V peak output limit. This limit is the best choice to allow for temperature variations of the diode and minimum output voltage specification.

APPLICATION INFORMATION

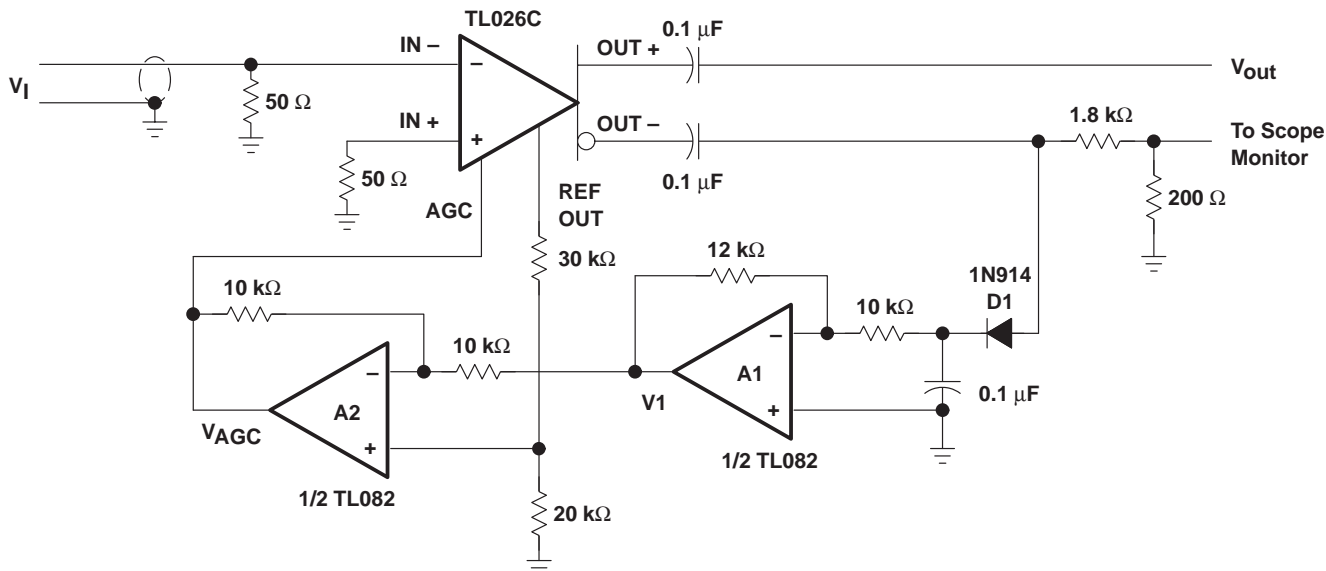
The circuit values in Figures 6 and 7 will produce the best results in this general application. Because of rectification and device input constraints, the circuit in Figure 6 will not provide attenuation and has about 32 dB of control range. The circuit shown in Figure 7 will have approximately 25% variation in the peak output voltage limit due to the variation in gain of the TL592 device to device. In addition, if a lower output voltage is desired, the output of the TL026C can be used for approximately 40 mV of controlled signal.

considerations for the use of the TL026C

To obtain the most reliable results, RF breadboarding techniques must be used. A groundplane board should be used and power supplies should be bypassed with 0.1- μ F capacitors. Input leads and output leads should be as short as possible and separated from each other.

A peak input voltage greater than 200 mV will begin to saturate the input stages of the TL026C and, while the circuit is in the AGC mode, the output signal may become distorted.

To observe the output signal of TL026C or TL592, low-capacitance FET probes or the output voltage divider technique shown in Figure 6 should be used.



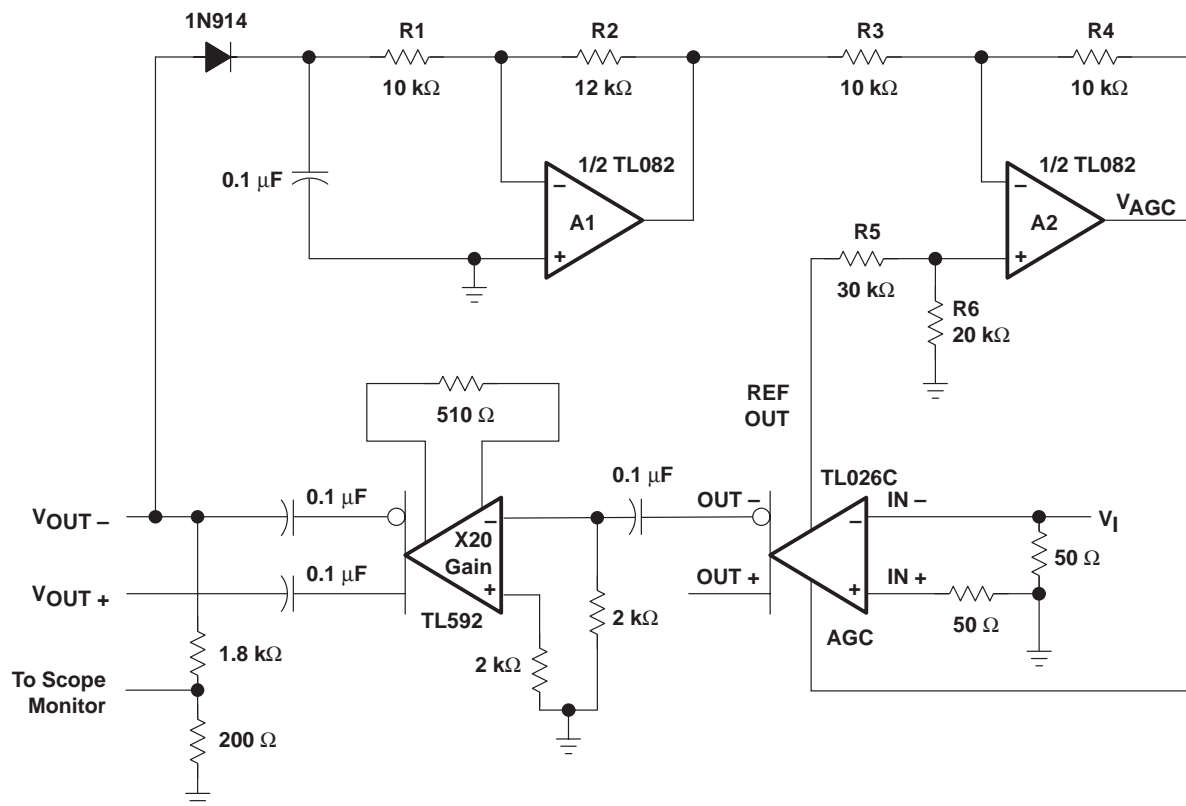
NOTE: $V_{CC+} = 6\text{ V}$ and $V_{CC-} = -6\text{ V}$ for TL026C and amplifiers A1 and A2.

Figure 6. Typical Application Circuit With No Attenuation

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NOTE: $V_{CC+} = 6\text{ V}$ and $V_{CC-} = -6\text{ V}$ for TL026C and amplifiers A1 and A2.

Figure 7. Typical Application Circuit With Attenuation

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